## CITY OF BLANCO

## PRELIMINARY INVESTIGATIONS AND REPORT WASTEWATER COLLECTION SYSTEM IMPROVEMENTS FOR PROPOSED SERVICE AREA

January 2, 2020


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## EXECUTIVE SUMMARY

This technical memorandum has been prepared to identify future wastewater flows and infrastructure needs within the proposed service area outlined in Exhibit A. This memorandum focuses on the development south of Blanco River and does not include land use assumptions or flow projections north of the river or within the City limits.

In general the topography of the service area slopes west to east. The area south of Blanco River has primarily three watersheds. Exhibit B, the City's Wastewater Capital Improvement Plan (Jones-Heroy \& Associates) identifies three wastewater basins that complement this topography. This exhibit identifies the need for 4 wastewater lift stations south of Blanco River. In this preliminary investigation the concept of conveying the wastewater adjacent to US Hwy. 281 was investigated.

In developing this memorandum, existing data was reviewed to assist in the development of land use projections within the proposed service area. These land use projections and associated acreage were then used to develop average, peak and wet weather wastewater flows.

This alignment would require a 15 inch gravity interceptor and two lift stations to keep the depth of the gravity interceptor from exceeding 25 feet. In this study it's assumed that the second lift station would convey wastewater under Blanco River and discharge into the existing collection system and ultimately be conveyed to the wastewater treatment plant. The scope of this study did not verify if the existing collection system north of Blanco River has the capacity to accept these additional flows.

The engineer's opinion of probable construction cost was completed for two lift stations and a gravity interceptor. The construction cost estimate includes a engineering design fee of 25 percent of the construction cost and a contingency of 25 percent. The cost estimate does not include costs for easement acquisition, topographical survey, or geotechnical investigations. The assumptions and clarifications for the study and the infrastructure needs are summarized below and explained in greater detail within the memorandum.

## DESIGN PARAMETERS / ASSUMPTIONS / CONSIDERATIONS / FINDINGS

- Study area is limited to south of the Blanco River
- Proposed gravity interceptor alignment flows south to north along US Hwy. 281
- Study did not cover possible need of smaller lift stations to convey wastewater from the developed areas to the proposed alignment
- Wastewater flow generation within the City Limits was not included in this study
- This study did not verify if the existing collection system north of Blanco River has the capacity to accept additional flows identified in this study
- Cost estimate does not include costs for easement acquisition
- Infrastructure requirements
o Lift Station 1-0.9 mgd
o Lift Station 2-4.4 mgd
o 15 inch Gravity Wastewater Interceptor - 15,800 linear feet
- Engineers opinion of probable construction cost $\$ 5$ million
- Engineering design cost $\$ 1.25$ million


## BACKGROUND

This technical memorandum has been prepared to identify future wastewater flows and infrastructure needs within the proposed service area outlined in Exhibit A. This memorandum focuses on the development south of Blanco River and does not include land use assumptions or flow projections north of the river or within the City limits. The infrastructure assumptions for conveyance of the wastewater are schematic in nature with measurements taken from existing GIS platforms. The intended use of this memorandum is conceptual, no topographic survey, geotechnical investigations, or easement research has been performed in the preparation of this memorandum.

## DATA REVIEW

The following maps and records were used to assist with recognizing the study boundary area and the current land use and owner information. This information was then used to develop land use assumptions and projected growth.

1. Exhibit A - City of Blanco Water and Wastewater Service Area Map (Jones-Heroy, September 2018)
2. Exhibit B - City of Blanco Wastewater Capital Improvements Plan (Jones-Heroy, September 2018)
3. Blanco County Appraisal District www.blancocad.com
4. TPDES Permit Application - City of Blanco WWTP

## CITY OF BLANCO TPDES PERMIT

The City of Blanco currently operates under a 0.225 MGD Texas Pollutant Discharge Elimination System (TPDES) wastewater permit. A permit "Renewal and Major Amendment" application has been submitted to the Texas Commission on Environmental Quality (TCEQ) for review. This amendment proposes a new wastewater treatment plant on the existing site. The proposed capacities of the permit amendment are broken into three phases as noted below. Phase I, the current permitted capacity of 0.225 MGD is currently in operation.
Permit Renewal and Major Amendment
City of Blanco 0.225 MGD Wastewater Treatment Plant
TPDES Permit No.: 10549002
Engineer: Darren C. Strozewski, P.E.
Applicant: City of Blanco

Phase I $\quad 0.225$ MGD (existing permit)
Phase II $\quad 0.950$ MGD (Amendment)
Phase III $\quad 1.60$ MGD (Amendment)

The information below is quoted from Section O "Explanation of the Need for Proposed Permit" of the permit renewal and modification application.
"Current City limits encompass approximately 1,400 acres of which a substantial portion is currently undeveloped or under developed. This 1,400 acres conservatively yields 1,400 wastewater service connections at one unit per acre, which equals 0.315 mgd using an average daily flow of 225 gallons per connection. In addition, the City's wastewater service area has been expanded by approximately 8,500 acres of privately owned land located adjacent to the City limits. This area is anticipated to develop as economic conditions continue to improve and when regional wastewater and water, and reclaimed water capacities are readily available from the City. The future 8,500 acre wastewater service area would conservatively yield 8,500 new wastewater service connections at one unit per acre, which equals 1.912 mgd using an average daily flow of 225 gallons per connection. Thus, the total wastewater service area capacity is 2.227 mgd .

This statement defines the future development within the City Limits to be limited to 225 gallons per acre. This assumption does not take into account commercial or high density residential development within the City limits.

## LAND USE PROJECTIONS

Land use must be identified in order to calculate projected wastewater flows. In this memorandum, the area assessed is limited to the proposed service area shown in Exhibit A and is limited to south of the Blanco River and does not take into consideration the land within the City Limits. Land use assumptions were determined based on current development, the vicinity to the City Limits, and commercial verses private ownership. In order to group like areas the proposed service area was subdivided into 14 smaller areas. For residential homes it was assumed that the larger lots 2-6 acres would vary due to topography and individual ownership, an average of 4 acres per lot was used in the calculations. A color coded Map of how these areas were zoned for the wastewater flow development are shown on Exhibit C. Appendix A shows a more detailed breakdown of each area indicating percentages of residential and commercial categories. The percentages of each type of land use are summarized on the next page.

## LAND USE BREAKDOWN

## Residential

Single Family Home, $1 / 4$ Acre Lots .............. 22.8\%

Single Family Home 2-6 Acre Lots............ 37.4\%
Multi Family.......................................................... $7.2 \%$
Commercial
Motel with kitchen................................................ 0.
Shopping Center .............................................-. $5.1 \%$
Restaurant ............................................................
Office...................................................................... $5.0 \%$
Industrial Building..................................................
Kennels/Stables ...............................................-2.9\%
Other (no wastewater flows were generated from the following land uses)
Agriculture/Ranch/Farm................................... 0.7
Park Land 9.9\%

## WASTEWATER FLOW PROJECTIONS

The wastewater flow projections were developed based on land use and acreage. The Average Dry Weather Flows (ADWF) were developed based on guidelines by TCEQ Chapter 217, Design Organic Loadings and Flows for New Wastewater Treatment Facilities https://www.tceq.texas.gov/assets/public/legal/rules/rules/pdflib/217c.pdf, and the 10 State Standards. The developed flows used for this study are summarized below.

| Average Dry Weather Flow (ADWF) (Qad) |  |  |
| :---: | :---: | :---: |
| Residential | Flow | Description |
| Single Family Home 1/4 Acre Lot | 245 gpd per home | $70 \mathrm{gpd} \mathrm{pp}$,3.5 persons per home. 1/4 acre lot |
| Single Family Home 2-6 Acre Lot | 280 gpd per home | $80 \mathrm{gpd} \mathrm{pp}, 3.5$ persons per home, 2-6 acre lot |
| Multi Family | 1,950 gpd per acre | $65 \mathrm{gpd} \mathrm{pp}, 1.5$ persons per unit, 20 units per acre |
| Commercial | Flow | Description |
| Motel with kitchen | 2,000 gpd per acre | 100 gpd per unit, 20 units per acre |
| Shopping Center | 164 gpd per acre | $12 \mathrm{gpd} /$ employee, $2 \mathrm{gpd} / 2$ parking spaces, 12 employees/ AC , 20 parking spaces AC |
| Restaurant | 600 gpd per acre | 3 gpd per meal, 200 meals per day |
| Office | 195 gpd per acre | 13 gpd per employee, 15 employees per AC |
| Industrial Building | 104 gpd per acre | 13 gpd per employee, 8 employee per AC |
| Kennels/Stables | 13 gpd per acre | 13 gpd per employee, 1 employee per AC |
| Park Land | 0 gpd per acre | No wastewater service provided |
| Private | Flow | Description |
| /Agriculture/Ranch/Farm | 0 gpd per acre | No wastewater service provided |

The average dry weather, peak dry weather and peak wet weather flows were calculated per the City of Austin design criteria for each area. These areas were summed accumulatively from the southern limits of the proposed service area to Blanco River and are included in Appendix B. The total accumulated flow for the proposed service area south of the river are shown below.

- Average Dry Weather Flow (ADWF) 0.5 mgd
- Peak Dry Weather Flow (PDWF) 2.2 mgd
- Peak Wet Weather Flow (PWWF) 4.4 mgd


## INFRASTRUCTURE DESIGN PARAMETERS

In general the topography of the service area slopes west to east. The area south of Blanco River has primarily three watersheds, one that flows to Flat Creek, one that flows to Durham Branch and one that flows directly to the Blanco River. Flat Creek and Durham Branch ultimately confluence with the Blanco River just east and outside of the proposed service area. Exhibit B, the City's Wastewater Capital Improvement Plan (CIP) (Jones-Heroy \& Associates) identifies three wastewater basins that complement this topography. The Exhibit B identifies the need for 4 wastewater lift stations south of Blanco River.

In this preliminary investigation the concept of conveying the wastewater adjacent to US Hwy. 281 was investigated. This alignment would require a Lift Station (LS 1) north of Flat Creek to convey flows over the ridge and into the next watershed that conveys flow to Durham Branch and a Lift Station (LS 2) north of Durham Branch to convey flows over the next ridge and ultimately under the Blanco River. In this study it's assumed that the discharge from LS 2 (north of Blanco River) would discharge into the existing collection system and ultimately be conveyed to the wastewater treatment plant. Exhibit D shows the schematic representation of this alignment.

If the capacity of the existing collection system (north of the river) is not sufficient a new gravity interceptor or a lift station and forcemain or combination thereof would be required. Cost for infrastructure north of Blanco River is outside the scope of this report.

- Lift Station 1 (north of Flat Creek)
o Design flow 680 gpm
o Submersible Duplex
o Wet Well $12^{\prime}$ dia. X $30^{\prime}$ deep
o Pumps (2) $40 \mathrm{HP}, 460 \mathrm{~V} 3 \mathrm{PH}, 60 \mathrm{~Hz}$, ( 680 gpm @ 100' TDH)
- Lift Station 2 (north of Durham Branch)
o Design flow 3098 gpm
o Submersible Triplex
o Wet Well $24^{\prime}$ dia. X $40^{\prime}$ deep
o Pumps (3) $60 \mathrm{HP}, 460 \mathrm{~V} 3 \mathrm{PH}, 60 \mathrm{~Hz}$, (2,850 gpm @ 100' TDH 2 pumps running)
Gravity interceptor flow capacities were calculated per the City of Austin and TCEQ design standards with a slope of $1 \%$. Using this design criteria a 12 inch gravity interceptor would be required at the beginning of the alignment and it would transition into a 15 inch interceptor south of the intersection of RR 32. With this alternative depths of the gravity interceptor did not exceed 20 feet. Lift Station 2 identified at Durham Branch could possibly be replaced with a siphon however this option is not included in the scope of this study.


## WATER REUSE

If the wastewater generated in this study was to be treated and returned to the same service area the TPDES permit would need to be revised and wider easements would need to be obtained to account for the required 10 foot separation from the wastewater line and surrounding water lines. The infrastructure required for this would include a new reclaimed water delivery system including pumping, elevated storage, pipe lines and associated appurtenances. The design for this system is outside the scope if this study. A conservative estimate for the construction of the pipe line only would be approximately $\$ 70$ per linear foot. Using the same footage of wastewater interceptor ( 15,800 If) would equate to a construction cost of $\$ 1,106,000$. Costs for easement acquisition, survey, geotechnical investigations, design and the construction of the delivery system would also need to be included.

Reclaimed water line construction cost \$1.1 million*
*cost does not include design, survey, geotechnical investigations, easement acquisition or construction cost for pump station/elevated storage.

## COST ESTIMATES

Engineers Opinion of Probable Construction cost is include in Appendix C. This construction cost estimate is based on the wastewater infrastructure identified in the previous section of this report. For economic and future capacity reasons a 15 inch interceptor was used for the entire reach. The construction cost estimate includes a contingency of 25 percent. A cost for engineering, survey, and geotechnical investigations was included at $25 \%$ of the construction cost.

Engineers Opinion of Probable Construction Cost \$5.6 million*
Engineering design, survey and geotechnical investigations
\$1.25 million*
*cost does not include easement acquisition

## EXHIBITS

Exhibit A - City of Blanco Water and Wastewater Service Area Map (Jones-Heroy, September 2018)
Exhibit B - City of Blanco Wastewater Capital Improvements Plan (Jones-Heroy, September 2018)
Exhibit C - Land Use Assumptions

## APPENDICES

Appendix A - Land Use Assumptions
Appendix B - Wastewater Flow Calculations

Appendix C - Engineers Opinion of Probable Construction Cost

## EXHIBIT A



## EXHIBIT B



## EXHIBIT C

LAND USE MAP


12/10/2019, 4:32:20 PM

| 1:31,279 |  |  |  |
| :---: | :---: | :---: | :---: |
| 0 | 0.35 | 0.7 | 1.4 mi |
| 0 | 0.5 | 1 |  |

## EXHIBIT C

## LAND USE MAP

## APPENDIX A

| AREA 1-HH FAMILY INVESTMENTS II LTD |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |
| PROPERTY ID | LEGAL DESCRIPTION | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 9198 | ABS A1300 SURVEY $21 / 2$ PAULINE JONAS,ACRES 30.75 | 30.75 | AC |  |  |  |
| 9197 | ABS A0983 SURVEY 74 A. BECKMAN,ACRES 35.0 | 35.00 | AC |  |  |  |
| 9199 | ABS A1299 SURVEY 167 1/2 PAULINE JONAS,ACRES 12.5 | 12.50 | AC |  |  |  |
| 9193 | ABS A1070 SURVEY 81 F. Vollmering, ACRES 21.5 | 21.50 | AC |  |  |  |
| 8561 | ABS A1070 SURVEY 81 F . VOLLMERING,ACRES 79.91,(MO RANCH) | 79.91 | AC |  |  |  |
| 9189 | ABS A0622 SURVEY 167 J WILSON,ACRES 316.96 | 316.96 | AC |  |  |  |
| 8559 | ABS A0582 SURVEY 168 Q.C. STEPHANS,ACRES 62.4,(MO RANCH) | 62.40 | AC |  |  |  |
| 2279 | ABS A0582 SURVEY 168 Q.C. STEPHANS,ACRES 34.292 | 34.20 | AC |  |  |  |
| 9200 | ABS A0827 SURVEY 161 FRIEDRICH MULLER,ACRES 145.0 | 145.00 | AC |  |  |  |
| 9195 | ABS A0632 SURVEY 93 W.C. WINTERS,ACRES 42.13 | 42.10 | AC |  |  |  |
| 3224 | ABS A0582 SURVEY 168 Q.C. STEPHANS,ACRES 1.46 | 1.46 | AC |  |  |  |
| 3225 | ABS A0582 SURVEY 168 Q.C. STEPHANS,ACRES 1.375 | 1.30 | AC |  |  |  |
| 14968 | ABS A0622 SURVEY 167 J WILLON,ACRES 3.04 | 3.40 | AC |  |  |  |
| 14969 | ABS A0582 SURVEY 168 Q.C. STEPHANS,ACRES 9.16 | 9.16 | AC |  |  |  |
| 15847 | BLANCO VISTA ESTATES, LOT 01, ACRES 5.01 | 5.00 | AC |  |  |  |
| 15848 | BLANCO VISTA ESTATES, LOT 02, ACRES 5.01 | 5.00 | AC |  |  |  |
| 9188 | ABS A1058 SURVEY 30 AUGUST JONAS,ACRES 56.75 | 11.35 | AC |  |  | a portion (20\%) of lot in inside of proposed service area boundary |
| 9194 | ABS A0696 SURVEY 73 HENDERSON \& OBRR CO.,ACRES 320.0 | 0.00 | AC |  |  | adjacent to but outside of proposed service area boundary |
| 9187 | ABS A0333 SURVEY 724 SOPHIA JONAS,ACRES 43.0 | 0.00 | AC |  |  | adjacent to but outside of proposed service area boundary |
|  | Total | 816.99 | AC |  |  |  |
|  |  | 122.55 | AC | 15\% | PARK LAND |  |
|  |  | 138.89 | AC | 17\% | INDUSTRIAL | Frontage along US 281 |
|  |  | 490.19 | AC | 60\% | SF RESIDENTS, 2-6 AC LOTS |  |
|  |  | 65.36 |  | 8\% | OFFICE |  |
|  |  |  |  | 100\% |  |  |
|  |  | 123 | LOTS |  | 4 AC LOTS |  |
|  |  |  |  |  |  |  |
| AREA 2 - BLANCO VISTA ESTATES (BLANCO VISTA DR) |  |  |  |  |  |  |
| PROPERTY ID | LeGAL DESCRIPTION | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 15850 | BLANCO VISTA ESTATES , LOT 04, ACRES 5.06 | 5.05 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15851 | BLANCO VISTA ESTATES, LOT 05 , ACRES 5.28 | 5.28 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15852 | BLANCO VISTA ESTATES, LOT 06, ACRES 5.47 | 5.47 | AC |  | LUXURY RESIDENTS 2-6 AC Lots |  |
| 15853 | BLANCO VISTA ESTATES , LOT 07 , ACRES 5.34 | 5.34 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15854 | BLANCO VISTA ESTATES, LOT 08, ACRES 5.01 | 5.01 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15855 | blanco vista estates, LOT 09, ACRES 5.07 | 5.07 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15856 | bLANCO VISTA ESTATES, LOT 10 , ACRES 5.3 | 5.30 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15857 | BLANCO VISTA ESTATES, LOT 11 , ACRES 5.33 | 5.33 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 15858 | BLANCO VISTA ESTATES , LOT 12 , ACRES 5.68 | 5.68 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 16146 | BLANCO VISTA ESTATES, LOT 13 \& 14, ACRES 10.91 | 10.91 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 16147 | ? | 0.00 | AC |  | LUXURY RESIDENTS 2-6 AC LOTS |  |
| 16148 | BLANCO VISTA ESTATES, LOT 15 , ACRES 11.26, Undivided Interest 42.0000 | 11.26 | AC |  | OFFICE |  |
| 16149 | BLANCO VISTA ESTATES, LOT 16, ACRES 11.26, Undivided Interest 42.0000 | 11.26 | AC |  | OFFICE |  |
| 16150 | BLANCO VISTA ESTATES, LOT 17 , ACRES 10.0, Undivided Interest 42.00000 | 10.00 | AC |  | SHOPS |  |
| 16151 | BLANCO VISTA ESTATES, LOT 18 , ACRES 10.0, Undivided Interest 42.00000 | 10.00 | AC |  | SHOPS |  |
| - | TOTAL | 100.96 | AC |  |  |  |
|  |  | 21.20 | AC | 21\% | OFFICES |  |
|  |  | 21.20 | AC | 21\% | SHOPPING |  |
|  |  | 58.56 | AC | 58\% | SF RESIDENTS 2-6 AC LOTS |  |
|  |  |  |  | 100\% |  |  |
|  |  | 11 | LOTS |  | EXISTING 5-10 AC LOTS |  |
|  |  |  |  |  |  |  |


| AREA 3-ABS A0632 | EY 93 W.C.WINTERS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PROPERTY ID | LEGAL DESCRIPTION |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 14911 | ABS A0632 SURVEY 93 W.C. WINTERS,ACRES 115.305 |  | 115.31 | AC |  | STABLES | 50\% DEVELOPED WITH RANCH HOUSE AND STABLES |
| 14068 | ABS A0632 SURVEY 93 W.C. WINTERS,ACRES 46.92 |  | 46.92 | AC |  | STABLES | LAND LOCKED |
|  |  | TOTAL | 162.23 | AC |  |  |  |
|  |  |  | 12.98 | AC | 8\% | SF RESIDENTS 6 AC LOT |  |
|  |  |  | 74.62 | AC | 46\% | AGRICULTURE/STABLES |  |
|  |  |  | 74.62 | AC | 46\% | INDUSTRIAL |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 1 | LOT |  | EXISTING RESIDENTS |  |
|  |  |  |  |  |  |  |  |
| AREA 4 - BRADLEY HA | E ESTATE |  |  |  |  |  |  |
| PROPERTY ID | LEGAL DESCRIPTION |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 4006 | ABS A0827 SURVEY 161 FRIEDRICH MULLER,ACRES 15.0 |  | 15.00 | AC |  |  |  |
| 14141 | ABS A0970 SURVEY 2 J.W. SPEER,ACRES 59.0 |  | 59.00 | AC |  |  |  |
| 14140 | ABS A0314 SURVEY 1 INDIANOLO RR CO,ACRES 126.0 |  | 126.00 | AC |  |  |  |
|  |  | TOTAL | 200.00 | AC |  |  |  |
|  |  |  | 30.00 | AC | 15\% | PARK LAND |  |
|  |  |  | 0.00 | AC | 0\% | Office |  |
|  |  |  | 170.00 | AC | 85\% | SF RESIDENCE 1/4 AC LOTS |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 680 | LOTS |  | 1/4 AC LOTS |  |
|  |  |  |  |  |  |  |  |
| AREA 5- BECKMANN | MITHERMAN |  |  |  |  |  |  |
| PROPERTY ID | LEGAL DESCRIPTION |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 10736 | ABS A0399 SURVEY 94 JOHN McCLENCHENON,ACRES 558.63 |  | 558.63 | AC |  |  |  |
|  |  | TOTAL | 558.63 | AC |  |  |  |
|  |  |  | 83.79 | AC | 20\% | PARK LAND |  |
|  |  |  | 223.45 | AC | 40\% | SF RESIDENTS 2-6 AC LOTS |  |
|  |  |  | 223.45 | AC | 40\% | SF RESIDENCE 1/4 AC LOTS |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 894 | LOTS |  | 1/4 AC LOTS |  |
|  |  |  | 56 | LOTS |  | 4 AC LOTS |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| AREA 6-ABS A0591 | EY 92 WM. N. TRAINER (WEST OF 281) |  |  |  |  |  |  |
| PROPERTY ID | legal description |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 14436 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 1.9 |  | 0.00 | AC |  | PRIVATE ROAD |  |
| 16627 | AbS A0591 SURVEY 92 Wm. N. TRAINER,ACRES 11.11 |  | 11.11 | AC |  | INDUSTRIAL WITH RESIDENTS |  |
| 4038 | AbS A0591 SURVEY 92 WM. N. TRAINER,ACRES 13.76 |  | 13.76 | AC |  | INDUSTRIAL WITH RESIDENTS |  |
| 4465 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 6.96 |  | 6.96 | AC |  | INDUSTRIAL WITH RESIDENTS |  |
| 10904 | ABS A0591 SURVEY 92 Wm. N. TRAINER,ACRES 3.913 |  | 3.91 | AC |  | INDUSTRIAL WITH RESIDENTS |  |
| 7994 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 6.64 |  | 6.64 | AC |  | KENNEL WITH RESIDENTS |  |
|  |  | TOTAL | 42.38 | AC |  |  |  |
|  |  |  | 0.00 | AC | 0\% | LUXURY RESIDENTS 4 AC LOTS |  |
|  |  |  | 0.00 | AC | 0\% | SHOPPING |  |
|  |  |  | 36.03 | AC | 85\% | INDUSTRIAL |  |
|  |  |  | 6 | AC | 15\% | KENNEL |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 5 | LOTS |  | 2-6 AC LOTS |  |
|  |  |  |  |  |  |  |  |


| AREA 7- DALEY PHILP |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PROPERTY ID | LeGAl description |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 3270 | ABS A0314 SURVEY 1 INDIANOLO RR CO,ACRES 283.21 |  | 283.21 | AC |  |  |  |
| 14435 | AbS A0314 SURVEY 1 INDIANOLO RR CO,ACRES 8.0 |  | 8.00 | AC |  |  |  |
|  |  | TOTAL | 291.21 | AC |  |  |  |
|  |  |  | 0.00 | AC | 0\% | AGRICULTURE/RANCH/FARM |  |
|  |  |  | 0.00 | AC | 0\% | LUXURY RESIDENTS, 2-6 AC LOTS |  |
|  |  |  | 116.48 | AC | 40\% | SINGLE FAMILY RESIDENTS 1/4 AC LOTS |  |
|  |  |  | 116.48 | AC | 40\% | MULTI-FAMILY RESIDENTS |  |
|  |  |  | 0.00 | AC | 0\% | MOTEL WITH KITCHEN |  |
|  |  |  | 0.00 | AC | 0\% | RESTAURANT |  |
|  |  |  | 0.00 | AC | 0\% | SHOPPING |  |
|  |  |  | 0.00 | AC | 0\% | OFFICE |  |
|  |  |  | 0.00 | AC | 0\% | INDUSTRIAL |  |
|  |  |  | 0.00 | AC |  | STABLES/KENNELS |  |
|  |  |  | 58.24 | AC | 20\% | PARK LAND |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 466 | LOTS |  | 1/4 AC LOTS |  |
|  | , |  |  |  |  |  |  |
|  | - |  |  |  |  |  |  |
| AREA 8-ABS A0591 SUR | EY 92 WM. N. TRAINER (EAST OF 281) |  |  |  |  |  |  |
| PROPERTY ID | LEGAL DESCRIPTION |  | QTY | UNITS | PERCENT | PROPOSED LAND USE | COMMENTS |
| 3811 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 47.49 |  | 47.49 | AC |  | OfFICE |  |
| 14200 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 5.98 |  | 5.98 | AC |  | SHOPPING |  |
| 6808 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 5.0 |  | 5.00 | AC |  | LUXURY RESIDENTS |  |
| 3950 | AbS A0591 SURVEY 92 WM. N. TRAINER,ACRES 40.345, Undivided Inte | terest | 40.35 | AC |  | SHOPPING \& RESTAURANT |  |
| 19092 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 20.0,SN1 12402584A;H | ;HUD\# | 20.00 | AC |  | CHURCH (OFFICE) |  |
| 17817 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 24.043,SN1 12402584A | AA; HU | 24.04 | AC |  | MULTI FAMILY |  |
| 6023 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 40.0 |  | 40.00 | AC |  | SHOPPING AND RESTAURANT |  |
| 10714 | ABS A0591 SURVEY 92 WM. N. TRAINER,ACRES 8.37 |  | 8.37 | AC |  | MULTI FAMILY |  |
|  |  | TOTAL | 191.23 | AC |  |  |  |
|  |  |  | 0.00 | AC | 0\% | AGRICULTURE/RANCH/FARM |  |
|  |  |  | 0.00 | AC | 0\% | LUXURY RESIDENTS, 2-6 AC LOTS |  |
|  |  |  | 0.00 | AC | 0\% | SINGLE FAMILY RESIDENTS 1/4 AC LOTS |  |
|  |  |  | 28.68 | AC | 15\% | MULTI-FAMILY RESIDENTS |  |
|  |  |  | 13.39 | AC | 7\% | MOTEL WITH KITCHEN |  |
|  |  |  | 5.74 | AC | 3\% | RESTAURANT |  |
|  |  |  | 57.37 | AC | 30\% | SHOPPING |  |
|  |  |  | 47.81 | AC | 25\% | OFFICE |  |
|  |  |  | 0.00 | AC | 0\% | INDUSTRIAL |  |
|  |  |  | 0.00 | AC | 0\% | STABLES/KENNELS |  |
|  |  |  | 38.25 | AC | 20\% | PARK LAND |  |
|  |  |  |  |  | 100\% |  |  |
|  |  |  | 1 | LOT |  | 6 AC LOT |  |
|  |  |  |  |  |  |  |  |





## APPENDIX B

19,967.67 gpd
0.03089 cfs

PDWF 83,673.64 gpd
604,504.76 gpd
0.12946 cfs
0.93531 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 0.00 AC |  |  |
| Size of lots | 0.25 AC |  |  |
| Number of units | 0 Units |  |  |
| ADWF = |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | ---: |
| Residential Area | 490.19 AC |
| Size of lots | 4 AC |
| Number of units | 123 Units |
|  |  |
| ADWF $=\quad$ Units * 280 gpd |  |
| 0.44 gpd |  |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.50
Qpd = (PF*ADWF)
Qpd =
0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

```
Qpw = PDWF+|&|
\[
\begin{aligned}
I \& I & =367,645.50 \mathrm{gpd} \\
\text { Qpw } & =367,647.47 \mathrm{gpd}
\end{aligned}
\]
```

I\&I = $750 \mathrm{gpd} / \mathrm{acre}$

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :--- |
| Residential Area | 0.00 AC |

$$
\text { ADWF }=\quad \text { Area } * 1950 \mathrm{gpd}
$$

$$
\begin{array}{lll}
0.00 \mathrm{gpd} & 0.00 \mathrm{gpm} & 0.00000 \mathrm{cfs}
\end{array}
$$

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```


## Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $\|\&\|=$ |  |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

Motel with Kitchen
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 2000 gpd per acre |
| :--- | :--- |
| Area | 0.00 AC |

ADWF = Area * 2000 gpd
0.00 gpd $0.00 \mathrm{gpm} \quad 0.00000 \mathrm{cfs}$

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

## Shopping Center

Average Dry Weather Flow (ADWF) (Qad)

| Flow | 126 gpd per acre |
| :--- | :--- |
| Area | 0.00 AC |

ADWF $=\quad$ Area $* 126 \mathrm{gpd}$
0.00 gpd $\quad 0.00 \mathrm{gpm} \quad 0.00000 \mathrm{cfs}$

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

Restaurant
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 600 gpd per acre |
| :--- | :--- |
| Area | 0.00 AC |
|  |  |
| ADWF $=$ |  |
|  | Area * 600 gpd |
|  | 0.00 gpd |

$0.00 \mathrm{gpm} \quad 0.00000 \mathrm{cfs}$

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ | 0.00 gpd |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.16
Qpd = (PF*ADWF)
```

Qpd = 53,051.42 gpd $\quad 36.82 \mathrm{gpm} \quad 0.08203 \mathrm{cfs}$

Peak Wet Weather Flow (PWWF) (Qpw)

$$
\begin{array}{rlrl}
\text { Qpw } & =P D W+I \& I \\
\text { I\&I } & = & 49,019.40 \mathrm{gpd} \\
\text { Qpw } & = & 102,070.82 \mathrm{gpd}
\end{array}
$$

I\& $=750 \mathrm{gpd} / \mathrm{acre}$

Industrial
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  |  |
| :---: | :---: | :---: |
| Area |  | 138.8 |
| ADWF = | Area * 52 gpd |  |
|  | 7,222.19 |  |

5.01 gpm
0.01117 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.24
Qpd = (PF*ADWF)
Qpd = 30,620.25 gpd 0.04735 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ |
| ---: | :--- |
| $I \& I=$ | $104,166.23 \mathrm{gpd}$ |
| $Q p w=$ | $134,786.48 \mathrm{gpd}$ |

$|\&|=750$ gpd/acre
$\begin{aligned} \mid \& I & =104,166.23 \mathrm{gpd} \\ \text { Opw } & =134,786.48 \mathrm{gpd}\end{aligned}$
93.54 gpm
0.20841 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow | 13 gpd per acre |
| :--- | :--- |
| Area | 0.00 AC |

ADWF $=\quad$ Area $* 13$ gpd
0.00 gpd
0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm |

## Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

| ADWF | $6,805.75 \mathrm{gpd}$ | 0.01053 cfs |
| :--- | ---: | ---: |
| PDWF | $29,361.27 \mathrm{gpd}$ | 0.04543 cfs |
| PWWF | $105,081.27 \mathrm{gpd}$ | 0.16258 cfs |

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.18 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ | $I \& I=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $43,917.60 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $43,917.78 \mathrm{gpd}$ | 30.48 gpm |

Multi Family Residential Homes, 20 units per AC Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| $Q p w$ | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=\quad 0.00 \mathrm{gpd}$
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Area |  | 21.20 AC |  |  |
| ADWF = | Area * 126 gpd |  |  |  |
|  | 2,671.40 gpd |  | 1.85 gpm | 0.00413 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.34$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=11,585.78 \mathrm{gpd}$ | 8.04 gpm | 0.01791 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- |
| $I \& I$ | $=15,901.20 \mathrm{gpd}$ |
| Qpw | $=\quad 27,486.98 \mathrm{gpd}$ |

|\&|=750 gpd/acre

Qpw $=\quad 27,486.98$ gpd
19.08 gpm
0.04250 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 195 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 21.20 AC |
| ADWF = | Area * 195 gpd |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.30$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=17,775.31 \mathrm{gpd}$ | 12.34 gpm | 0.02748 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $15,901.20 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $33,676.51 \mathrm{gpd}$ | 23.37 gpm |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | :--- |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area * 52 gpd |  |
|  | 0.00 gpd |  |}

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | $4,850.53 \mathrm{gpd}$ | 0.00750 cfs |
| :--- | ---: | ---: |
| PDWF | $20,975.03 \mathrm{gpd}$ | 0.03245 cfs |
| PWWF | $142,643.78 \mathrm{gpd}$ | 0.22070 cfs |

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} / \mathrm{acre}$ |  |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 12.98 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 1 Units | changed to 1 due to existing development |  |
| ADWF = Units * 280 gpd |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.02 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ | $I \& I=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $9,733.50 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $9,733.52 \mathrm{gpd}$ | 6.76 gpm |

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |


| ADWF $=$ | Area 1950 gpd |
| ---: | :--- | ---: |
| 0.00 gpd |  |$\quad 0.00 \mathrm{gpm} \quad 0.00000 \mathrm{cfs}$

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | PDWF $+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+(0.0206 * \mathrm{ADWF})^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 52 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 74.62 AC |
| ADWF = | Area * 52 gpd |  |
|  | 3,880.42 |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.31$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=\quad 16,706.65 \mathrm{gpd}$ |

11.59 gpm
0.02583 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=55,967.63 \mathrm{gpd}$ |  |
| Qpw | $=$ | $72,674.27 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre
Qpw $=\quad 72,674.27 \mathrm{gpd}$
50.44 gpm
0.11237 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

0.67 gpm
0.00150 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.40$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=4,268.37 \mathrm{gpd}$ | 2.96 gpm | 0.00660 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $55,967.63 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $60,235.99 \mathrm{gpd}$ | 41.80 gpm |


| ADWF | 2.78 gpd |
| :--- | ---: |
| PDWF | 12.47 gpd |
| PWWF | $127,512.47 \mathrm{gpd}$ |

0.00000 cfs 0.00002 cfs 0.19729 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | ---: |
| Residential Area | 170.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 680 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 2.78 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.49$ |  |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |  |
| Qpd | $=$ | 12.47 gpd | 0.01 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=127,500.00 \mathrm{gpd}$ |
| Qpw | $=127,512.47 \mathrm{gpd}$ |

$\& \&=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=127,512.47$ gpd
88.49 gpm
0.19716 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 0.00 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 0 Units |  |  |
| ADWF = |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00 \mathrm{gpd}$
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |


| ADWF $=$ |  |  |
| ---: | :--- | ---: |
|  | 1950 gpd <br> 0.00 gpd | 0.00 gpm |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | PDWF $+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00 \mathrm{gp}$
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+(0.0206 * \mathrm{ADWF})^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | 3.85 gpd |
| :--- | ---: |
| PDWF | 17.29 gpd |
| PWWF | $335,195.29 \mathrm{gpd}$ |

0.00001 cfs 0.00003 cfs 0.51862 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | ---: |
| Residential Area | 223.45 AC |
| Size of lots | 0.25 AC |
| Number of units | 894 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| $\quad 3.65$ gpd |  |

0.00 gpm
0.00001 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.49$ |  |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |  |
| Qpd | $=16.39 \mathrm{gpd}$ | 0.01 gpm | 0.00003 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | $167,589.00 \mathrm{gpd}$ |
| Qpw | $=$ | $167,605.39 \mathrm{gpd}$ |

$\& \&=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=167,605.39$ gpd
116.32 gpm
0.25916 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 223.45 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 56 Units |  |  |
| ADWF $=\quad$ Units * 280 gpd |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.90 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- | ---: |
| $I \& I$ | $=167,589.00 \mathrm{gpd}$ |
| Qpw | $=\quad 167,589.90 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre
apw $=167,589.90$ gpd
116.31 gpm
0.25913 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |


| ADWF $=$ |  |  |
| ---: | :--- | ---: |
|  | 1950 gpd <br> 0.00 gpd | 0.00 gpm |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | PDWF $+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | $1,955.98 \mathrm{gpd}$ |
| :--- | ---: |
| PDWF | $8,541.72 \mathrm{gpd}$ |
| PWWF | $40,328.97 \mathrm{gpd}$ |

0.00303 cfs 0.01322 cfs 0.06240 cfs

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

|\&| = $750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 0.00 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 0 Units |  |  |
| ADWF $=\quad$ Units * 280 gpd |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 1950 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Residential |  | 0.00 AC |  |  |
| ADWF = Area * 1950 gpd |  |  |  |  |
|  | 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | PDWF $+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| $Q p w$ | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |
| ---: | :--- |
| $I \& I$ | $=$ |
| Qpw | $=$ |$\quad 0.00 \mathrm{gpd}$

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = 0.00 gpd
0.00 gpm
0.00000 cfs
ADWF $=\quad$ Area $* 600 \mathrm{gpd}$
0.00 gpd $0.00 \mathrm{gpm} \quad 0.00000 \mathrm{cfs}$

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206**ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.50
Qpd = (PF*ADWF)
Qpd = 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |
| ---: | :--- |
| $I \& I$ | $=$ |
| Qpw | $=$ |
|  | 0.00 gpd |
|  | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00 \mathrm{gpd}$
0.00 gpm
0.00000 cfs

Office
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 195 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Area |  | 0.00 AC |  |  |
| ADWF = | Area * 195 gpd |  |  |  |
|  | 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

Industrial
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  |  |
| :---: | :---: | :---: |
| Area |  | 36.0 |
| ADWF = | Area * 52 gpd |  |
|  | 1,873.33 |  |

1.30 gpm
0.00290 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.36$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=8,172.27 \mathrm{gpd}$ | 5.67 gpm | 0.01264 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | $27,019.16 \mathrm{gpd}$ |
| Qpw | $=$ | $35,191.43 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 35,191.43$ gpd
$24.42 \mathrm{gpm} \quad 0.05441 \mathrm{cfs}$

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 6.36 AC |
| ADWF = | Area * 13 gpd |  |

82.65 gpd
0.06 gpm
0.00013 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.47$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=369.45 \mathrm{gpd}$ | 0.26 gpm | 0.00057 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $4,768.09 \mathrm{gpd}$ |  |  |
| Qpw |  | $5,137.53 \mathrm{gpd}$ | 3.57 gpm |


| ADWF | $227,145.70 \mathrm{gpd}$ |
| :--- | :--- |
| PDWF | $775,237.96 \mathrm{gpd}$ |
| PWWF | $949,963.96 \mathrm{gpd}$ |

0.35145 cfs
1.19947 cfs
1.46981 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | ---: |
| Residential Area | 116.48 AC |
| Size of lots | 0.25 AC |
| Number of units | 466 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 1.90 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)
$\left.P F=\left(18+\left(0.0206^{*} A D W F\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} A D W F\right)^{\wedge} 0.5\right)$
$\mathrm{PF}=\quad 4.50$

Qpd = (PF*ADWF)
$\begin{array}{lll}\text { Qpd }= & 8.55 \mathrm{gpd} & 0.01 \mathrm{gpm} \\ 0.00001 \mathrm{cfs}\end{array}$
Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=87,363.00 \mathrm{gpd}$ |
| Qpw | $=87,371.55 \mathrm{gpd}$ |

I\& $=750$ gpd/acre

Qpw = 87,371.55 gpd
60.64 gpm
0.13510 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |
| Size of lots | 4 AC |
| Number of units | 0 Units |


| ADWF $=$ | Units * 280 gpd |  |
| ---: | :--- | ---: |
| 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=0.00$ gpd
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

Flow | 1950 gpd per acre |
| :--- |
| Residential Area |
|  |
| ADWF $=\quad$ Area * 116.48 AC |
| $227,143.80$ gpd |

0.35122 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=3.41$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=775,229.41 \mathrm{gpd}$ | 538.01 gpm | 1.19869 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |
| ---: | :--- |
| $I \& I$ | $=87,363.00 \mathrm{gpc}$ |
| Qpw | $=862,592.41 \mathrm{gpc}$ |

$|\&|=750$ gpd/acre

Qpw = 862,592.41 gpd
598.64 gpm
1.33377 cfs

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$
0.00 gpm
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+(0.0206 * \mathrm{ADWF})^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | $102,699.00 \mathrm{gpd}$ |
| :--- | :--- |
| PDWF | $408,580.99 \mathrm{gpd}$ |
| PWWF | $523,317.79 \mathrm{gpd}$ |

0.15890 cfs 0.63217 cfs 0.80969 cfs

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)
$\left.P F=\left(18+\left(0.0206^{*} A D W F\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} A D W F\right)^{\wedge} 0.5\right)$
$\mathrm{PF}=\quad 4.50$

Qpd = (PF*ADWF)
$\begin{array}{lll}\text { Qpd }= & 0.00 \mathrm{gpd} & 0.00 \mathrm{gpm} \\ 0.00000 \mathrm{cfs}\end{array}$
Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- |
| $I \& I$ | $=r \quad 0.00 \mathrm{gpd}$ |
| Qpw | $=$ |

I\& $=750$ gpd/acre

Qpw $=\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |
| Size of lots | 4 AC |
| Number of units | 0 Units |


| $\mathrm{ADWF}=$ | Units $* 280 \mathrm{gpd}$ |  |
| ---: | :--- | ---: |
| 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC Average Dry Weather Flow (ADWF) (Qad)

38.82 gpm
0.08649 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=3.86$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=\quad 215,934.38 \mathrm{gpd}$ | 149.86 gpm | 0.33389 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | $21,513.15 \mathrm{gpd}$ |
| Qpw | $=$ | $237,447.53 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=237,447.53 \mathrm{gpd}$
164.79 gpm
0.36715 cfs

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.03$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=107,922.46 \mathrm{gpd}$ | 74.90 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $10,039.47 \mathrm{gpd}$ | 81.87 gpm | 0.18240 cfs |

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206**ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF = 4.24
Qpd = (PF*ADWF)
Qpd= 30,645.90 gpd 21.27 gpm 0.04739 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=43,026.30 \mathrm{gpd}$ |  |
| Qpw | $=$ | $73,672.20 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = 73,672.20 gpd
0.11391 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 5.74 AC |
| ADWF = | Area * 600 gpd |  |
|  | 3,442.10 |  |

2.39 gpm
0.00532 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.32$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=14,856.45 \mathrm{gpd}$ | 10.31 gpm | 0.02297 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ | $I \& I=750 \mathrm{gpd} /$ acre |  |
| ---: | ---: | ---: | ---: |
| $I \& I=$ | $4,302.63 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $19,159.08 \mathrm{gpd}$ |  |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.21$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=39,221.79 \mathrm{gpd}$ | 27.22 gpm | 0.06065 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw = | F+ I\& | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| :---: | :---: | :---: | :---: |
| I\&I = | 35,855.25 gpd |  |  |
| Qpw = | 75,077.04 gpd | 52.10 gpm | 0.11609 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=\quad 0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 13 gpd per acre |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Area | 0.00 AC |  |  |  |
|  |  |  |  |  |
| ADWF $=$ | Area $* 13 \mathrm{gpd}$ |  |  |  |
| 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

| ADWF | $140,319.56 \mathrm{gpd}$ |
| :--- | :--- |
| PDWF | $507,706.82 \mathrm{gpd}$ |
| PWWF | $577,344.32 \mathrm{gpd}$ |

0.21711 cfs 0.78554 cfs 0.89328 cfs

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

|\&| = $750 \mathrm{gpd} /$ acre

Qpw = $\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 0.00 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 0 Units |  |  |
| ADWF $=\quad$ Units * 280 gpd |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC Average Dry Weather Flow (ADWF) (Qad)

94.24 gpm
0.20997 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=3.60$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=488,285.13 \mathrm{gpd}$ | 338.87 gpm | 0.75501 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |
| ---: | :--- |
| $I \& I$ | $=52,228.13 \mathrm{gpd}$ |
| Qpw | $=540,513.26 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=540,513.26$ gpd
375.12 gpm
0.83576 cfs

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Area |  | 0.00 AC |  |  |
| ADWF = | Area * 126 gpd |  |  |  |
|  | 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$
0.00 gpm
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 195 gpd per acre |
| :--- | :--- | :--- |
| Area |  |  |
|  |  |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.29$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=19,421.69 \mathrm{gpd}$ | 13.48 gpm | 0.03003 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $17,409.38 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $36,831.06 \mathrm{gpd}$ | 25.56 gpm |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF $=$ | Area * 13 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |


| ADWF | $1,810.65 \mathrm{gpd}$ |
| :--- | ---: |
| PDWF | $7,902.89 \mathrm{gpd}$ |
| PWWF | $77,540.39 \mathrm{gpd}$ |

0.00280 cfs 0.01223 cfs 0.11997 cfs

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)
$\left.P F=\left(18+\left(0.0206^{*} A D W F\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} A D W F\right)^{\wedge} 0.5\right)$
$\mathrm{PF}=\quad 4.50$

Qpd = $\left(P F^{*} A D W F\right)$
$\begin{array}{lll}\text { Qpd }= & 0.00 \mathrm{gpd} & 0.00 \mathrm{gpm} \\ 0.00000 \mathrm{cfs}\end{array}$
Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- |
| $I \& I$ | $=r \quad 0.00 \mathrm{gpd}$ |
| Opw | $=$ |

I\& $=750$ gpd/acre

Qpw $=\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | :---: |
| Residential Area | 83.57 AC |
| Size of lots | 4 AC |
| Number of units | 21 Units |

## ADWF = Units * 280 gpd

0.07 gpd
0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

```
                PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
                PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.34 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | $62,673.75 \mathrm{gpd}$ |
| Qpw | $=$ | $62,674.09 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre
apw $=62,674.09$ gpd
0.09691 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :---: |
| Residential Area | 0.00 AC |


| ADWF $=$ |  |  |
| ---: | :--- | ---: |
|  | 1950 gpd <br> 0.00 gpd | 0.00 gpm |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | PDWF $+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$ 0.00 gpm
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 195 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 9.29 AC |  |  |
| ADWF = | Area * 195 gpd |  |  |  |
|  | 1,810.58 gpd |  | 1.26 gpm | 0.00280 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.36$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=7,902.56 \mathrm{gpd}$ | 5.48 gpm | 0.01222 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | ---: | ---: | :--- |
| I\&I $=$ | $6,963.75 \mathrm{gpd}$ |  |  |
| Qpw $=$ | $14,866.31 \mathrm{gpd}$ | 10.32 gpm | 0.02299 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=\quad 0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF $=$ | Area * 13 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | 887.64 gpd |
| :--- | ---: |
| PDWF | $3,909.28 \mathrm{gpd}$ |
| PWWF | $16,711.78 \mathrm{gpd}$ |

0.00137 cfs 0.00605 cfs 0.02586 cfs

Single Family Residential Homes, 1/4 AC lots

## Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :---: |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 0.00 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 0 Units |  |  |
| ADWF = |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.00 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw = $\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :--- |
| Residential Area | 0.00 AC |
|  |  |
| ADWF $=\quad$ Area * 1950 gpd |  |
| 0.00 gpd |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |  |
| Qpd | $=(\mathrm{PF}$ *ADWF) |  |  |
| Qpd | $=0.00 \mathrm{gpd}$ | 0.00 gpm | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$ 0.00 gpm
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

| Average Dry Weather Flow (ADWF) (Qad) |  |  |
| :---: | :---: | :---: |
| Flow |  | 52 gpd per acre |
| Area |  | 17.07 AC |
| ADWF = | Area * 52 gpd |  |
|  | 887.64 |  |

0.62 gpm
0.00137 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.40$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=3,909.28 \mathrm{gpd}$ | 2.71 gpm | 0.00604 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=12,802.50 \mathrm{gpd}$ |  |
| Qpw | $=$ | $16,711.78 \mathrm{gpd}$ |

$|\&|=750$ gpd/acre

Qpw $=16,711.78$ gpd

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF $=$ | Area * 13 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | $85,181.07 \mathrm{gpd}$ |
| :--- | ---: |
| PDWF | $338,260.47 \mathrm{gpd}$ |
| PWWF | $690,039.72 \mathrm{gpd}$ |

0.13179 cfs
0.52337 cfs
1.06765 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :---: |
| Residential Area | 211.07 AC |
| Size of lots | 0.25 AC |
| Number of units | 844 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| $\quad 3.45$ gpd |  |

0.00 gpm
0.00001 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+(0.0206 * \mathrm{ADWF})^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.49$ |  |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |  |
| Qpd | $=$ | 15.49 gpd | 0.01 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- |
| $I \& I$ | $=158,300.66 \mathrm{gpd}$ |
| $Q p w$ | $=$ |
|  | $158,316.15 \mathrm{gpd}$ |

|\&| = 750 gpd/acre

Qpw = $158,316.15$ gpd
109.87 gpm
0.24479 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |  |  |
| :---: | :---: | :---: | :---: |
| Residential Area | 164.16 AC |  |  |
| Size of lots | 4 AC |  |  |
| Number of units | 41 Units |  |  |
| ADWF = |  |  |  |
|  |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.66 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | $123,122.74 \mathrm{gpd}$ |
| Qpw | $=$ | $123,123.40 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=123,123.40 \mathrm{gpd}$
85.45 gpm
0.19038 cfs

Multi Family Residential Homes, 20 units per AC Average Dry Weather Flow (ADWF) (Qad)

| Flow <br> Residential Area |  |  |
| :---: | :---: | :---: |
|  |  | 28.1 |
| ADWF = |  |  |

38.09 gpm
0.08485 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=3.87$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=\quad 212,127.94 \mathrm{gpd}$ | 147.22 gpm | 0.32800 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W+\|\&\|$ |
| ---: | :--- |
| $I \& I$ | $=$ |
| Qpw | $=$ |
|  | $23,106.76 \mathrm{gpd}$ |
|  |  |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 233,234.69$ gpd
161.86 gpm
0.36064 cfs

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.10$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=76,899.57 \mathrm{gpd}$ | 53.37 gpm | 0.11891 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| $I \& I=$ | $7,035.59 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $83,935.15 \mathrm{gpd}$ | 58.25 gpm |

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Area |  | 46.90 AC |  |  |
| ADWF = | Area * 126 gpd |  |  |  |
|  | 5,909.89 gpd |  | 4.10 gpm | 0.00914 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.26$ |  |  |
| Qpd | $=\left(\right.$ PF $\left.^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=\quad 25,193.23 \mathrm{gpd}$ | 17.48 gpm | 0.03895 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=35,177.93 \mathrm{gpd}$ |  |
| Qpw | $=$ | $60,371.15 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Opw = 60,37115 gpd
41.90 gpm
0.09335 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 9.38 AC |
| ADWF = | Area * 600 gpd |  |
|  | 5,628.47 |  |

3.91 gpm
0.00870 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.27$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=\quad 24,023.59 \mathrm{gpd}$ | 16.67 gpm | 0.03715 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw = | F+ I\& | $\|\&\|=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| :---: | :---: | :---: | :---: |
| I\& = | 7,035.59 gpd |  |  |
| Qpw = | $31,059.17 \mathrm{gpd}$ | 21.56 gpm | 0.04802 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)

| Flow <br> Area |  | 195 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 0.00 AC |  |  |
| ADWF = | Area * 195 gpd |  |  |  |
|  | 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=\quad 0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Stables/Kennels
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | $5,710.91 \mathrm{gpd}$ |
| :--- | ---: |
| PDWF | $24,366.73 \mathrm{gpd}$ |
| PWWF | $177,314.98 \mathrm{gpd}$ |

0.00884 cfs 0.03770 cfs 0.27435 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | ---: |
| Residential Area | 45.32 AC |
| Size of lots | 0.25 AC |
| Number of units | 181 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.74 gpd |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=3.33 \mathrm{gpd}$ | 0.00 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |
| ---: | :--- | ---: |
| $I \& I$ | $=33,988.50 \mathrm{gpd}$ |
| Qpw | $=\quad 33,991.83 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw $=\quad 33,991.83 \mathrm{gpd}$
23.59 gpm
0.05256 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | :---: |
| Residential Area | 113.30 AC |
| Size of lots | 4 AC |
| Number of units | 28 Units |

## ADWF $=\quad$ Units $* 280$ gpd

0.10 gpd
0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.46 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=84,971.25 \mathrm{gpd}$ |  |
| Qpw | $=$ | $84,971.71 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 84,971.71 \mathrm{gpd}$
58.97 gpm
0.13139 cfs

Multi Family Residential Homes, 20 units per AC Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 1950 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Resident |  | 0.00 AC |  |  |
| ADWF $=$ | Area * 1950 gpd |  |  |  |
|  | 0.00 gpd |  | 0.00 gpm | 0.00000 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw | $=$ | 0.00 gpd | 0.00 gpm |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Area |  | 45.32 AC |  |  |
| ADWF = | Area * 126 gpd |  |  |  |
|  | 5,710.07 gpd |  | 3.96 gpm | 0.00883 cfs |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.27$ |  |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |  |
| Qpd | $=24,362.95 \mathrm{gpd}$ | 16.91 gpm | 0.03767 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=33,988.50 \mathrm{gpd}$ |  |
| Qpw | $=$ | $58,351.45 \mathrm{gpd}$ |

|\& $=750$ gpd/acre

Qpw = 58,351.45 gpd
0.09023 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |
| Qpd | $=0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 13 gpd |  |
|  |  |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF}$ *ADWF $)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |


| ADWF | 195.75 gpd |
| :--- | ---: |
| PDWF | 871.96 gpd |
| PWWF | $94,936.96 \mathrm{gpd}$ |

0.00030 cfs 0.00135 cfs 0.14689 cfs

Single Family Residential Homes, 1/4 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 245 gpd per home |
| :--- | :--- |
| Residential Area | 0.00 AC |
| Size of lots | 0.25 AC |
| Number of units | 0 Units |
|  |  |
| ADWF $=\quad$ Units * 245 gpd |  |
| 0.00 gpd |  |

0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)
$\left.P F=\left(18+\left(0.0206^{*} A D W F\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} A D W F\right)^{\wedge} 0.5\right)$
$\mathrm{PF}=\quad 4.50$

Qpd = (PF*ADWF)
$\begin{array}{lll}\text { Qpd }= & 0.00 \mathrm{gpd} & 0.00 \mathrm{gpm} \\ 0.00000 \mathrm{cfs}\end{array}$
Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+\|\&\|$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

|\&| = $750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$ gpd 0.00 gpm
0.00000 cfs

Single Family Residential Homes, 2-6 AC lots
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 280 gpd per acre |
| :--- | :---: |
| Residential Area | 110.37 AC |
| Size of lots | 4 AC |
| Number of units | 28 Units |

## ADWF = Units * 280 gpd

0.10 gpd
0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

```
PF = (18+(0.0206*ADWF)^0.5)/(4+0.0206*ADWF)^0.5)
PF= 4.50
Qpd = (PF*ADWF)
Qpd= 0.44 gpd 0.00 gpm 0.00000 cfs
```

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=82,777.20 \mathrm{gpd}$ |  |
| Qpw | $=$ | $82,777.64 \mathrm{gpd}$ |

$|\&|=750 \mathrm{gpd} /$ acre
57.45 gpm
0.12799 cfs

Multi Family Residential Homes, 20 units per AC
Average Dry Weather Flow (ADWF) (Qad)

| Flow | 1950 gpd per acre |
| :--- | :--- |
| Residential Area | 0.00 AC |
|  |  |
| ADWF $=\quad$ Area * 1950 gpd |  |
| 0.00 gpd |  |

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& I=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I$ | $=$ |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

## Motel with Kitchen

Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750$ gpd/acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

Shopping Center
Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 126 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 126 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& I$ |  |
| ---: | :--- | ---: | :--- |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} / \mathrm{acre}$

Qpw = $\quad 0.00$ 0.00 gpm
0.00000 cfs

## Restaurant

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 600 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 0.00 AC |
| ADWF = | Area * 600 gpd |  |
|  | 0.00 |  |

0.00 gpm
0.00000 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.50$ |  |
| Qpd | $=(\mathrm{PF} * \mathrm{ADWF})$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} / \mathrm{acre}$ |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Office
Average Dry Weather Flow (ADWF) (Qad)


Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: | :--- |
| PF | $=4.50$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=0.00 \mathrm{gpm}$ | 0.00000 cfs |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw $=$ | $P D W F+I \& \mid$ | $\|\&\|=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | :--- | :--- |
| $I \& I=$ | 0.00 gpd |  |  |
| Qpw $=$ | 0.00 gpd | 0.00 gpm | 0.00000 cfs |

Industrial

\section*{Average Dry Weather Flow (ADWF) (Qad) <br> | Flow |  | 52 gpd per acre |
| :--- | :--- | ---: |
| Area |  | 0.00 AC |
|  |  |  |
| ADWF $=$ | Area $* 52 \mathrm{gpd}$ |  |
|  | 0.00 gpd |  |}

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |
| ---: | :--- |
| PF | $=4.50$ |
| Qpd | $=\left(\mathrm{PF}{ }^{*} \mathrm{ADWF}\right)$ |
| Qpd | $=\quad 0.00 \mathrm{gpd}$ |

0.00 gpm
0.00000 cfs

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ |  |
| ---: | :--- | ---: |
| $I \& I$ | $=$ | 0.00 gpd |
| Qpw | $=$ | 0.00 gpd |

$|\&|=750 \mathrm{gpd} /$ acre

Qpw $=\quad 0.00$ gpd
0.00 gpm
0.00000 cfs

## Stables/Kennels

Average Dry Weather Flow (ADWF) (Qad)

| Flow |  | 13 gpd per acre |
| :---: | :---: | :---: |
| Area |  | 15.05 AC |
| ADWF = | Area * 13 gpd |  |
|  | 195.66 |  |

0.14 gpm
0.00030 cfs

Peak Dry Weather Flow (PDWF) (Qpd)

| PF | $\left.=\left(18+\left(0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right) /\left(4+0.0206^{*} \mathrm{ADWF}\right)^{\wedge} 0.5\right)$ |  |
| ---: | :--- | ---: |
| PF | $=4.45$ |  |
| Qpd | $=\left(\mathrm{PF}^{*} \mathrm{ADWF}\right)$ |  |
| Qpd | $=871.51 \mathrm{gpd}$ | 0.60 gpm |

Peak Wet Weather Flow (PWWF) (Qpw)

| Qpw | $=P D W F+I \& \mid$ | $I \& \mid=750 \mathrm{gpd} /$ acre |  |
| ---: | :--- | ---: | :--- |
| I\&I | $=11,287.80 \mathrm{gpd}$ |  |  |
| Qpw | $=$ | $12,159.31 \mathrm{gpd}$ | 8.44 gpm |

## APPENDIX C

| CITY OF BLANCO |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WASTEWATER TRUNK MAIN |  |  |  |  |  |  |  |
| PRELIMINARY ENGINEER'S OPINION OF PROBABLE PROJECT COST |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  | :11-18-2019 |
| NO. | DESCRIPTION | UNIT | QTY |  | RICE |  | OUNT |
|  |  |  |  |  |  |  |  |
| WASTEWATER INTERCEPTOR |  |  |  |  |  |  |  |
|  | PIPE, 15" PVC SDR 26 (ALL DEPTHS INCLUDING EXCAVATION \& BACKFILL) | LF | 15,800 | \$ | 90 | \$ | 1,422,000 |
|  | JACK \& BORE , 24" PIPE 3/8" STEEL UNDER 281 (2PL) | LF | 750 | \$ | 800 | \$ | 600,000 |
|  | STANDARD PRE-CAST MANHOLE 5 FOOT DIAMETER (EVERY 700 FT) | EA | 23 | \$ | 11,550 | \$ | 260,700 |
|  |  |  |  |  |  |  |  |
| LIFT STATION NO. 1 |  |  |  |  |  |  |  |
|  | LIFT STATION DUPLEX 30' DEEP | LS | 1 | \$ | 192,050 | \$ | 192,050 |
|  | WET WELL \& PIPING |  |  |  |  |  |  |
|  | PUMPS (2) KSB MODEL E100-317/304XEG-S 40 HP, 460V 3 PHASE 60 HZ |  |  |  |  |  |  |
|  | EXPLOSION PROOF, ELEC SUBMERSIBLE PUMPS |  |  |  |  |  |  |
|  | 50' POWER CABLES, SS LIFTING BAILS, 35' SS LIFTING CHAIN |  |  |  |  |  |  |
|  | 48"X72" SINGLE DOOR ALUMINUM ACCESS COVER PEDESTRIAN LOADING |  |  |  |  |  |  |
|  | DUPLEX CONSTANT SPEED CONTROL PANEL |  |  |  |  |  |  |
|  | PRE-CAST VALVE VAULT | LS | 1 | \$ | 55,000 | \$ | 55,000 |
|  | SWING CHECK VALVES 8" | EA | 2 | \$ | 3,750 | \$ | 7,500 |
|  | PLUG VALVES 8" | EA | 3 | \$ | 1,750 | \$ | 5,250 |
|  | 2" ARAV | EA | 1 | \$ | 1,200 | \$ | 1,200 |
|  | FLOW METER \& VAULT | LS | 1 | \$ | 15,000 | \$ | 15,000 |
|  | STANDBY GENERATOR W CONCRETE PAD | LS | 1 | \$ | 75,000 | \$ | 75,000 |
|  | ELECTRICAL: CONTROL PANEL, ATS, MAIN DISCONNECT, SUBMERSIBLE TRANSDUCER, SCADA | LS | 1 | \$ | 70,000 | \$ | 70,000 |
|  | PIPE, 6" DUCTILE IRON FORCE MAIN AND FITTINGS | LF | 1,000 | \$ | 100 | \$ | 100,000 |
|  | JIB CRAIN AND TROLLEY | LS | 1 | \$ | 40,000 | \$ | 40,000 |
|  | ASPHALT DRIVE | SY | 50 | \$ | 100 | \$ | 5,000 |
|  | CHAIN LINK FENCE W/ 16' WIDE DBL SWING GATE | LF | 240 | \$ | 100 | \$ | 24,000 |
|  |  |  |  |  |  |  |  |
| LIFT STATION NO. 2 |  |  |  |  |  |  |  |
|  | LIFT STATION TRIPLEX 40' DEEP | LS | 1 | \$ | 186,772 | \$ | 186,772 |
|  | WET WELL \& PIPING | LS | 1 | \$ | 80,000 | \$ | 80,000 |
|  | PUMPS (3) KSB MODEL K150-317/454XEG-S 60 HP, 460V 3 PHASE 60 HZ |  |  |  |  |  |  |
|  | EXPLOSION PROOF, ELEC SUBMERSIBLE PUMPS |  |  |  |  |  |  |
|  | 65' POWER CABLES, SS LIFTING BAILS, 45' SS LIFTING CHAIN |  |  |  |  |  |  |
|  | (3) 36 "X48" SINGLE DOOR ALUMINUM ACCESS COVER PEDESTRIAN LOADING |  |  |  |  |  |  |
|  | DUPLEX CONSTANT SPEED CONTROL PANEL |  |  |  |  |  |  |
|  | PRE-CAST VALVE VAULT | LS | 1 | \$ | 55,000 | \$ | 55,000 |
|  | SWING CHECK VALVES 8" | EA | 2 | \$ | 3,750 | \$ | 7,500 |
|  | PLUG VALVES 8" | EA | 3 | \$ | 1,750 | \$ | 5,250 |
|  | 2" ARAV | EA | 1 | \$ | 1,200 | \$ | 1,200 |
|  | FLOW METER \& VAULT | LS | 1 | \$ | 15,000 | \$ | 15,000 |
|  | STANDBY GENERATOR W CONCRETE PAD | LS | 1 | \$ | 75,000 | \$ | 75,000 |
|  | ELECTRICAL: CONTROL PANEL, ATS, MAIN DISCONNECT, SUBMERSIBLE TRANSDUCER, SCADA | LS | 1 | \$ | 75,000 | \$ | 75,000 |
|  | PIPE, 8" DUCTILE IRON FORCE MAIN AND FITTINGS | LF | 1,000 | \$ | 110 | \$ | 110,000 |
|  | JIB CRAIN AND TROLLEY | LS | 1 | \$ | 40,000 | \$ | 40,000 |
|  | ASPHALT DRIVE | SY | 50 | \$ | 100 | \$ | 5,000 |
|  | CHAIN LINK FENCE W/ 16' WIDE DBL SWING GATE | LF | 275 | \$ | 100 | \$ | 27,500 |
|  |  |  |  |  |  |  |  |
| SITE CIVIL WORK |  |  |  |  |  |  |  |
|  | SITE WORK - CLEARING AND GRUBBING | LS | 1 | \$ | 78,000 | \$ | 78,000 |
|  | SHEET SHORING AND BRACING | LS | 1 | \$ | 75,000 | \$ | 75,000 |
|  | TRENCH EXCAVATION SAFETY SYSTEM ALL DEPTHS | LF | 5,800 | \$ | 5 | \$ | 29,000 |
|  | SILT FENCE FOR EROSION CONTROL | LF | 4,000 | \$ | 5 | \$ | 20,000 |
|  | NATIVE GRASSLAND SEEDING AND PLANTING | SY | 4,000 | \$ | 6 | \$ | 24,000 |
|  | BARRICADES, SIGNS \& TRAFFIC HANDLING | MON | 3 | \$ | 4,000 | \$ | 12,000 |
|  | STABILIZED CONSTRUCTION ENTRANCE | EA | 2 | \$ | 2,000 | \$ | 4,000 |
|  | TREE PROTECTIVE FENCING, TYPE A, CHAIN LINK FENCE, INCLUDING BOARDS FOR TREE TRUNK PROTECTION | LF | 1,000 | \$ | 5 | \$ | 5,000 |
|  | STORM WATER POLLUTION PLAN | LS | 1 | \$ | 6,000 | \$ | 6,000 |
|  | MOBILIZATION, BONDS, INSURANCE, SUBMITTALS, DEMOBILIZATION AND CLOSEOUT, COMPLETE IN PLACE | LS | 1 | \$ | 190,446 | \$ | 190,446.08 |
|  |  |  |  |  |  |  |  |
|  | SUBTOTAL |  |  |  |  | \$ | 3,999,368 |
|  | CONTINGENCIES (+/- 25\%) |  |  |  |  | \$ | 999,632 |
|  | TOTAL ESTIMATED CONSTRUCTION COST |  |  |  |  | \$ | 4,999,000 |
| NOTES |  |  |  |  |  |  |  |
|  | The Engineer has no control over the cost of labor, materials or equipment or over the Contractor(s) methods of determining |  |  |  |  |  |  |
|  | prices. The engineer not and does not guarantee the proposals, bids or construction costs will not vary from the opinion of |  |  |  |  |  |  |
|  | probable cost prepared by him. |  |  |  |  |  |  |
| 2 This estimate does not include right-of-way or easement acquisition. |  |  |  |  |  |  |  |

